WE are now in a position to figure needed to accommodate them. A current density of 1200 amperes per sq. in. would be sufficient for the primary in view of the high ratio of copper to insulation; this winding, however, has to carry the magnetising or "wattless" current as well as the equivalent of the secondary load, so that it may be well to reduce the current density to 1000 amperes per sq. in. or less. No. 18 S.W.G. has a sectional area of 0.00181 sq. in., and may therefore be relied on to carry 1.81 amperes; apart from the magnetising current, the primary will carry only a little over an ampere, so that this wire is entirely suitable. No. 18 D.C.C. winds 17 turns per inch, so that 670 turns will require

sq. in., or 2.32 sq. inches.

Each half of the high-voltage winding carries current only half the time. so that the wire may be smaller than would otherwise be the case. Actually 28 S.W.G. proves sufficient, and it is recommended that either double cotton covered or single cotton enamelled wire be used. Even so, for absolute safety it is desirable to put a layer of good paper (varnished when in position) or oiled silk between each two layers of the winding. At 3 turns per volt, the 1000 volts right across the winding will require 3000 turns which, since 28 D.C.C. winds 39 turns to the inch, will take up approximate 2 square inches. The grid bias winding may be of No. 36 D.C.C. and will take un about .25 of a square inch.

out the various windings and de- which may be either one or two Mar- these windings. termine what window space will be coni or Osram US full-wave rectifiers. or two or four UX 281 half-wave rectifiers, may be fed from 22 turns of No. 14 D.C.C., which will take up another .25 of a square inch. The rectifiers for the grid-bias will no doubt be 5-6 volt 201a type valves, and may have their filaments fed from 16 turns layers of the high-voltage windings, if of No. .22 D.C.C. or larger wire.

The total cross-sectional area of the windings is, then, 2.32 + 2 + .25 +.25 + .25 + .5 square inches, or a total of 5.57 square inches. The winding bobbin, the air-space between it and the core, the insulation between windings and the insulation between the any is used, will all take up space, and The power-valve filaments will rea a "window" area of 8 square inches will quire, if of the 250 or 210 type, 22 be none too great. Efficient design de-

## A POWER PACK FOR "250" VALVES

### FINE ARTICLE COMMENCES NEXT WEEK

IN our next issue "Megohm" will commence a description of a power pack which will deliver 450 volts and ample current for six or seven valves. This power pack has been so described that almost everything can be built by the home constructor. This so that no increase in wire diameter will be a special issue—do not miss it!

### 

turns of No. 14 D.C.C. taking up .25 mands that the "yokes" should be apa.c. valves in the earlier stages No. 12 D.C.C. will be needed, the number of turns depending on the valves employed; if 4 volt a.c. valves are employed 12 turns will be needed. Some constructors would prefer, perhaps wisely, to make provision for all three

of a square inch. For feeding several preciably shorter than the legs on which the windings are mounted, so that suitable dimensions for the window will be 4 inches by 2 inches.

#### The Iron Required.

A LITTLE figuring shows that the iron required will be as follows: types of a.c. valves, so that it will be If .014 stalloy (handled by Johns,

The filaments of the rectifier valves, wise to allow 5 of a square inch for Ltd., Auckland) is used, there will be needed 160 pieces 5%in, by 2in., 268 pieces 4in, by 1fin., and 108 pieces 54in. by 1 3-16in, or, if the suppliers object to the odd size, 54in. by 14in. If .018 Stalloy (handled by National Electrical and Engineer Co., Wellington) is used, there will be required 126 pieces 5şin. by 2in., 212 pieces 4in. by 1şin., and 86 pieces 54in. by 1 3-16in., or 14in. It must not be forgotten, when assembling the core, that the joins in the laminations must be staggered.

The mean length of the iron path is about 19 inches, and since it takes 10 ampere turns per inch to magnetise Stalloy to a flux density of 60,000 lines per square inch. 190 ampere turns will be called for for magnetising the core. The primary turns are 670 in number, so that the magnetising current is

- = 0.28 of an ampere.

Fortunately the 18 s.w.g. used in the primary will carry this "wattless" current in addition to the useful current. is called for.

The core contains about 16lb. of iron (1 cubic inch weighs 40z.) and the loss in Stalloy at the flux density mentioned is 0.7 watts per lb. Thus the iron loss will be about 10 watts.

Assuming that the secondaries are to be wound over the primary, the mean primary turn will be about 9 inches. Thus the primary will need nearly 4 lb. of No. 18 d.c.c., which will have a resistance of 2.2 ohms. The copper of  $1^2$  R loss in this winding will be, assuming the primary current to ne

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For those who desire to "sweep the world" the short wave section will be of undoubted assistance and the circuits and hints will help you to bring in all those stations your friends speak of so often.

Multi valve receivers are extensively dealt with, descriptive circuits are given of th most popular types, and full details re construction and tuning. The matter of maintenance is also dealt with in this section.

Perhaps the Glossary of Wireless Terms could be aptly described as one of the most helpful pages in the "Guide." Everything in radio is explained fully, even those wireless terms that have you tricked are dealt with in this

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